	Temperature (°K)	D	Molar volun	Molar volume (cm ³ /mole)		
		(kilobars)	Fluid	Solid 24.34±0.02	$\frac{\Delta V \text{ on melting}}{(\text{cm}^3/\text{mole})}$	
	94.73±0.02	0.451±0.007	27.30±0.02			
	94.74	0.459	27.31			
	100.76	0.721	26.89			
	108.12	1.051	26.52	24.02	2.50	
	110.77	1.186	26.32			
	120.85	1.674	25.85	23.65	2.20	
	140.88	2.708	24.96	23.04	1.92	
	160.40	3.805	24.26	22.54	1.72	
	180.15	4.999	23.65	22.08	1.57	
	180.20	5.003	23.66	22.11	1.55	
	201.32	6.335	23.10	21.69	1.41	

TABLE I. Experimental argon melting data.

 ± 1 bar at the lower pressures and ± 4 bar at the higher pressures. Construction of this gauge had not been completed at the time the measurements on the solid-fluid phase transition in argon were made, so a Heise Bourdon-tube pressure gauge with somewhat lower sensitivity and accuracy was used in these measurements. The resulting lower accuracy in the determination of the melting pressures will soon be rectified by high-precision measurements of pressure versus temperature along the melting curve for argon and other substances, which are in progress in this laboratory.

The volume of the argon sample was determined by a method not commonly used, but which has several desirable features. In the "normal" data runs the weight of the fluid occupying the entire vessel was measured as a function of pressure and tem-



FIG. 4. Isotherm through the solid-fluid phase transition in argon. Point A indicates a pressurization into the supercooled region before the argon began freezing in the vessel.

perature. In addition to these data runs another set of runs was made spanning the same pressure and temperature range, but this time with a solid iron cylinder filling most of the internal volume of the vessel. The difference between the weights of the fluid in the vessel at a given pressure and temperature with and without the iron cylinder in place is just the weight of a volume of the fluid equal to the volume of the iron cylinder at this pressure and temperature. Since this cylinder was subjected only to hydrostatic pressure, the small changes in its volume with pressure and temperature could be calculated accurately from the known equation of state of iron. Such a method for volume determination eliminates the need for assumptions concerning the behavior of a pressure vessel and its closure seals when the vessel is subjected to internal pressure. This is desirable since it was shown, at least for the pressure vessel being used in the present experiment, that the internal volume did not behave according to the usual assumptions.1

PROCEDURE AND RESULTS

Using the apparatus and techniques described above, P-V-T data were obtained for argon (99.995% pure). These data consist of several isotherms, each of which is made up of a number of equilibrium P-V-T points. The procedure for each isotherm, after the system had been initially pressurized, was first to pump a small amount of argon into the vessel or to release a small amount from it. The system was then allowed to equilibrate before the values of the pressure in the system and the temperature and weight of the vessel were recorded. This process was then repeated to obtain a series of points along the isotherm. Immediately after all the points for a particular isotherm

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TABLE II. Experimental $P-V-T$ data for fluid argon (P is in	n kilobars; V is in cubic centimeters per mole).
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210.16°Ka		190.73°K		170.36°K		150.73°K	
Р	V	Р	V	Р	V	P	V
$\begin{array}{c} 0.209\\ 0.277\\ 0.360\\ 0.437\\ 0.515\\ 0.598\\ 0.702\\ 0.782\\ 0.884\\ 0.977\\ 1.072\\ 1.195\\ 1.315\\ 1.320\\ \end{array}$	61.45 51.60 45.77 42.71 40.43 38.68 37.04 36.03 34.98 34.15 33.43 32.61 31.92	$\begin{array}{c} 0.203\\ 0.277\\ 0.348\\ 0.418\\ 0.483\\ 0.559\\ 0.633\\ 0.729\\ 0.824\\ 0.938\\ 1.044\\ 1.174\\ 1.299\\ 1.422\end{array}$	51.55 44.99 41.66 39.49 38.02 36.72 35.67 34.56 33.68 32.79 32.08 31.33 30.72 20.14	$\begin{array}{c} 0.209\\ 0.280\\ 0.347\\ 0.422\\ 0.489\\ 0.560\\ 0.634\\ 0.719\\ 0.820\\ 0.930\\ 1.051\\ 1.178\\ 1.311\\ 1.458\end{array}$	42.37 39.30 37.50 36.02 35.00 34.14 33.39 32.67 31.93 31.23 30.57 29.96 29.42 29.68	$\begin{array}{c} 0.212\\ 0.274\\ 0.341\\ 0.416\\ 0.489\\ 0.573\\ 0.664\\ 0.753\\ 0.854\\ 0.984\\ 1.112\\ 1.255\\ 1.412\\ 1.255\\ 1.412\\ 1.575\end{array}$	$\begin{array}{c} 36.79\\ 35.44\\ 34.35\\ 33.38\\ 32.62\\ 31.91\\ 31.25\\ 30.68\\ 30.12\\ 29.50\\ 28.96\\ 28.45\\ 27.95\\ 27.57\\ 50\\ 7.50\\ 7.50\\$
1.420 1.552 1.734 1.939 2.146 2.355 2.530	31.41 30.78 30.06 29.38 28.75 28.22 27.81	$ \begin{array}{r} 1.432 \\ 1.565 \\ 1.728 \\ 1.935 \\ 2.136 \\ 2.346 \\ 2.552 \\ \end{array} $	$\begin{array}{c} 30.14\\ 29.63\\ 29.07\\ 28.46\\ 27.93\\ 27.45\\ 27.03\end{array}$	$ \begin{array}{r} 1.438\\ 1.634\\ 1.829\\ 2.015\\ 2.220\\ 2.434\\ 2.648 \end{array} $	28.83 28.33 27.78 27.33 26.89 26.50 26.10	$ \begin{array}{r} 1.375\\ 1.754\\ 1.958\\ 2.153\\ 2.369\\ 2.605\\ 2.840 \end{array} $	27.05 27.05 26.63 26.25 25.86 25.48 25.14
2.759 3.035 3.306	27.33 26.83 26.37	2.776 3.026 3.261	26.61 26.18 25.83	2.914 3.179 3.450	25.69 25.31 24.94	3.115	24.77
3.577 3.839	25.99 25.61	3.554 3.835	25.42 25.07	3.726 4.000	24.62 24.31	P	V
4.123 4.462 4.806 5.143 5.484 5.823	25.26 24.88 24.53 24.22 23.95 23.67	4.139 4.478 4.797 5.134 5.486 5.561	24.72 24.37 24.07 23.78 23.50 23.43	4.301 <u>160.4</u> <u>P</u>	24.01 47°K V	0,208 0,291 0,380 0,459	34.84 33.53 32.47 31.75
6.160 6.464	23.42	180.	21°K	0.203	39.60	0.537	31.14 30.52
201.29°K		P	V	0.263 0.346	37.63 35.81	0.725 0.823	29.97 29.48
P	V	0.203 0.275	46.62 42.05	0.409 0.469 0.540 0.626	34.79 34.01 33.24 32.47	0.924 1.059 1.173 1.308	29.05 28.53 28.13 27.71
$\begin{array}{c} 0.205\\ 0.275\\ 0.348\\ 0.416\\ 0.493\\ 0.554\\ 0.624\\ 0.731\\ 0.838\\ 0.941\\ 1.041\\ 1.163\\ 1.266\\ 1.401\\ 1.550\\ 1.716\\ 1.938\\ 2.355\\ 2.566\\ 2.768\\ 3.002\\ 3.249\\ 3.517\\ 3.791\\ \end{array}$	57.20 48.50 44.12 41.55 39.48 38.24 37.08 35.69 34.58 33.68 32.95 32.18 31.59 30.93 30.28 29.66 28.95 27.86 27.86 27.40 27.01 26.60 26.20 25.80 25.44	$\begin{array}{c} 0.352\\ 0.424\\ 0.487\\ 0.553\\ 0.634\\ 0.724\\ 0.831\\ 0.935\\ 1.053\\ 1.053\\ 1.160\\ 1.282\\ 1.406\\ 1.554\\ 1.749\\ 1.949\\ 2.152\\ 2.355\\ 2.558\\ 2.787\\ 3.038\\ 3.316\\ 3.573\\ 3.871\\ 4.136\end{array}$	39.29 37.52 36.39 35.40 34.45 33.55 32.67 31.95 31.23 30.67 30.10 29.60 29.08 28.46 27.92 27.43 27.43 27.43 27.00 26.61 26.22 25.81 25.42 25.81 25.42 25.99 24.74 24.44	$\begin{array}{c} 0.728\\ 0.833\\ 0.939\\ 1.053\\ 1.184\\ 1.317\\ 1.454\\ 1.597\\ 1.728\\ 1.940\\ 2.148\\ 2.345\\ 2.562\\ 2.788\\ 3.041\\ 3.320\\ 3.582\\ 3.846\\ \end{array}$	31.09 31.02 30.42 29.88 29.30 28.82 28.37 27.96 27.59 27.09 26.64 26.26 25.90 25.54 25.18 24.82 24.50 24.22	1.445 1.589 1.756 1.939 2.114 2.310 2.524 2.720	21.35 26.98 26.58 26 21 25.88 25.55 25.22 24.95
4.130 4.458 4.806 5.150 5.488 5.824 6.203	25.03 24.67 24.33 24.03 23.74 23.47 23.47	4.444 4.738 4.916	24.14 23.86 23.71	s - Cut - Cut - Ti palitaint		28 28 29 190122 20 10 190122	

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